# Dealing with uncertainty



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# Engineers put trust in calculations

We have been calculating the probability of failure for safety functions for many years

Calculation results are presented confidently with precision:  $\mathsf{PFD}_{\mathsf{AVG}}\thickapprox3.15\times10^{\text{-}3}$  and  $\mathsf{RRF}\thickapprox317$ 

Sophisticated software shows us precisely how probability of failure will vary over time





# We have a challenge:

IEC 61511-1 Edition 2 added a new requirement, sub-clause 11.9.4:

*'reliability data uncertainties shall be assessed and taken into account when calculating the failure measure'* and sub-clause 11.4.9 requires that:

*'reliability data used in the calculation of failure measure shall be determined by an upper bound statistical confidence limit of no less than 70%'*

What does that mean in practice?

What uncertainty should we expect in reliability data?

How can we take that uncertainty into account?



# Measuring failure rate – the theory

Random failures have a **fixed and constant failure rate**

*If* a failure rate is reasonably constant, then the failure rate can be estimated from the **mean time between failures**:

 $\lambda$  ≈ 1/ MTBF

Mean time to failure (MTTF) may be used rather than MTBF, the difference is academic



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5

# Usage of MTBF and MTTF varies between references IEC 61508-6 and ISO 14224 have:

MTTF =  $1/\lambda = \tau/n$ , assuming repairs are 'as good as new'

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MTBF = MTTF + MTTR ≈ MTTF
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- MTTR = Mean time to restoration
- *n*= Number of failures observed
- $\tau$ = Aggregated time in service over which the failures were observed
- $\lambda$ = Failure rate - **valid for constant failure rate only**

ISO 14224 defines failure rate as the conditional probability per unit of time that the item fails between  $t$  and d $t$ , provided it has been working over [0, $t$ ]



# Time between failures follows a normal distribution

The time to failure of *individual* devices follows an exponential distribution if the failure events are **purely independent and random**

The time between failures measured in the overall population approximates a normal distribution around the MTBF

If that is valid, then a **chi-square function** can be used to estimate the true value of a failure rate λ with any desired level of confidence from the number of failures recorded



7

# λ can be estimated from any number of failures

The chi-square function uses only

 $\bullet$ Number of failures

$$
\lambda_{\alpha} = \frac{\chi^2(\alpha, \nu)}{2T}
$$

•Total time in service (device-hours)

 $\chi^2$  = chi-squared function

 $\alpha$  = 1- confidence level

 $v =$  degrees of freedom, in this case = 2.( $n + 1$ )

- *n* = the number of failures in the given time period
- *T* = the number of device-years or device-hours,
- i.e. the number of devices multiplied by the given time period



# Confidence levels and intervals from chi-square

- If an estimate is at the 70% **confidence level** there is a 30% chance that the true long term  $\lambda_\mathsf{AVG}$ will be worse (higher) than the estimate  $\lambda_{70\%}$
- $\bullet$  We can define a **confidence interval**: There is a 90% chance that the true long term  $\lambda_\mathsf{AVG}$ will be between  $\lambda_{5\%}$  and  $\lambda_{95\%}$



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9

Confidence interval width reduces with failure count The width of a confidence interval depends only on the number of failures recorded

It does not depend directly on the population size

λ can even be estimated with **zero** failures, based solely on the total time in service

Confidence in the estimate of a long-term average failure rate  $\lambda_\mathsf{AVG}$  improves as more failures are measured, i.e. the confidence interval becomes narrower



#### Confidence interval width reduces with failure count





# But this theory does not work in practice

The chi-squared function is only valid for **purely random events**  that can be characterised by a fixed and constant rate

Reality is more complicated

Few failures are purely random

We can always measure a historical average failure rate  $\lambda_\mathsf{AVG}$ but there is no single 'true' constant value to be measured



# What devices *might* have purely random failures?

- Sensor electronics
- Sensor process interfaces
- Logic solver electronics
- Variable speed drives
- Electrical relays or contactors
- Pneumatic or hydraulic devices **x**
- Actuated valvesS X



Refer to ISO/TR 12489 Annex B for explanation of random versus systematic failures



# What causes purely random failure?

- • Purely random behaviour is caused by a stochastic process, a series of **independent** events
- The impact of cosmic radiation on electronic components is stochastic, the rate of collisions is reasonably constant though not necessarily fixed at a single true value
- The failure rate might be reduced through radiation hardening or through fault detection and correction
- Components may be designed to withstand some damage; •eventually the component failure rate might increase over time as damage accumulates, i.e. no longer purely random $\frac{1}{\sqrt{2}}$



## Few failures are *purely* random

#### Most electronic component failures are **stress-related**: **Applied Stress vs Time**



After an illustration by Dr D. J. Smith in '*Reliability, Maintainability and Risk*'



# Applied stress can cause *quasi-*random failure

- $\bullet$ These failures are **dependent** on stress and strength
- • Typical stress factors include:
	- •**Temperature**
	- •**Shock**
	- •Vibration
	- Cyclic loading
	- •Voltage surge
- The failure rates may **appear to be** reasonably constant, but the failures are not due to stochastic processes



#### *All* failure rates can be expected to vary

For example, refer to IEC 61709:

#### *Electronic components – Reliability – Reference conditions for failure rates and stress models for conversion*

#### $\lambda = \lambda_{\text{ref}} \times \pi_1 \times \pi_1 \times \pi_{\text{T}} \times \pi_{\text{F}} \times \pi_{\text{S}} \times \pi_{\text{FS}}$

#### where

- is the failure rate under reference conditions:  $\lambda_{\text{ref}}$
- is the voltage dependence factor:  $\pi_{\text{L}}$
- is the current dependence factor;  $\pi_{\parallel}$
- is the temperature dependence factor;  $\pi_{\mathsf{T}}$
- is the environmental application factor;  $\pi_{\mathsf{F}}$
- $\pi_{\rm S}$ is the switching rate dependence factor;
- is the electrical stress dependence factor.  $\pi$ <sub>ES</sub>



# Failure rates vary across orders of magnitude

- The failure rates depend on the **magnitude** and **duration** of stress, and on design strength limits
- • Design strength depends on manufacturing methods, materials, tolerances, inspection, testing
- Failure rates may vary with an Arrhenius characteristic, strength degrades as damage accumulates over time
- Stress-related failure rates can be controlled by design, testing, and by reliability-centred preventive maintenance



# We can always measure MTBF

…**but the failure rate does not have a fixed constant value**

Failure rate is not an *inherent* characteristic of any device, it is a measure of its performance in a given environment

Confidence levels cannot be applied universally to failure rates, but we can instead consider **uncertainty** or **variability**



# Past performance reveals '**uncertainty'** interval width

Probability distributions can always be used to model **past** performance of any system, **random or not**

We can measure time between events and use statistical techniques to estimate the mean and variance in event rates

…but that does not mean that we can precisely predict **future** performance with confidence



## Is the probability of winning a coin toss constant?





# Probability distributions of coin toss trials **are constant**

- $\bullet$ The probability of tossing 'heads' is **fixed**
- $\bullet$ It is set by the balance and symmetry of the coin
- $\bullet$ The coin has no memory
- $\bullet$ Each toss is an independent event, purely random
- •Estimated mean and variance vary slightly between trials
- $\bullet$ The short term average varies, but…
- •The long term average is fixed and constant
- $\bullet$ Future performance can be predicted with some confidence



#### Probability distributions of coin toss trials are constant



## How does football club performance vary?





#### Football club performance varies from year to year



# Football club performance varies from year to year

The probability of winning each match *varies*, it depends on many systematic factors

- $\bullet$ Player ability
- $\bullet$ Coaching techniques
- $\bullet$ Training effectiveness
- $\bullet$ **Strategy**
- $\bullet$ Environment
- $\bullet$ Opposition ability
- $\bullet$ Ethical behaviour
- Good management



# Safety performance also depends on team effort

Equipment failure rates and safety incident rates depend on many influences such as

- •Design quality, including suitability for service
- $\bullet$ Installation
- $\bullet$ Accessibility for maintenance
- •Inspection and testing
- $\bullet$ Maintenance effectiveness
- $\bullet$ **Competence**
- $\bullet$ Environment
- Good management



# What proportion of safety-related failures are random?

Purely random failures are rarein industrial applications, typically  $< 1\%$ 





#### Failure rate is a performance indicator

Safety system performance is not **determined by** failure rates

Safety system performance **depends on team effort**

Failure rates are a **measure of** safety system performance



# Variability in reliability data is well understood

- Offshore Reliability Data OREDA established 1981, results first published in **1984**
- The 6<sup>th</sup> edition was published in 2015
- OREDA now includes onshore and offshore reliability data
- Different users record different failure rates
- Failure rates change over time with changing practices The rates typically vary over **2 or 3 orders of magnitude** OREDA summarises the mean and standard deviation as well as upper and lower deciles for equipment failure rates



# Typical variation

Variation in failure rates results from differences in application, environment and maintenance effectiveness Dr David J Smith published this summary in 2001:



Smith, D. J. *'Reliability, Maintainability and Risk'*, 6th Ed. Butterworth Heinemann. 2001



# Failure rates can be estimated at a 'certainty' level

Failure rates that are achieved by at least 70% of users can be estimated using readily available sources such as:

- $\bullet$ OREDA
- •*exida* Safety Equipment Reliability Handbook
- $\bullet$ FARADIP

Failure rates at around the 90% or 95% certainty level are typically a **factor of 3** higher than the 70% level



# Maintenance effectiveness

#### From Bukowski, J.V. and Stewart, L. : '*Quantifying the Impacts of Human Factors on Functional Safety*' American Institute of Chemical Engineers' 12th Global Congress on Process Safety, Houston, Texas. 2016

#### Ineffective maintenance results in probability of failure **3 or 4 times higher** than 'normal' maintenance practices

OREDA datasets are consistent with a similar conclusion:

 $\lambda_{95\%} \approx 3 \times \lambda_{70\%}$ 



# **Conclusions**

With site-specific data, we can expect that a 90% uncertainty interval spans *at least* one order of magnitude

#### **Worst case performance may be more than 3 times worse than 'normal'**

Best practice performance could be at least 3 times better than normal and maybe as much as 10 times better



# Achieving best practice

Failure performance depends on deliberate decisions and strategies applied to prevent preventable failures

Best practice performance can be achieved **at a cost** with **reliability centred maintenance** (e.g. aviation industry, defence industry)

Failure performance cannot be predicted with certainty because it depends on human behaviour



#### Failure probability estimates can never be precise

Probability of SIF Failure on Demand





# Back to our objective

*'reliability data uncertainties shall be assessed and taken into account when calculating the failure measure'*

A result such as  $\text{RRF}_{\text{AVG}}$  ≈ 317 could be expressed more realistically as:

 $\mathsf{RRF}_{\mathsf{AVG}}\thickapprox\:300$  if the maintenance is as effective as planned

though  $\mathsf{RRF}_{\mathsf{AVG}}$  may be < 100 if maintenance is not effective



# Should this level of uncertainty be acceptable?

Yes, of course, because risk and risk reduction targets can only be estimated to within half an order of magnitude at best

Uncertainty with a factor of > 3 is normal in risk assessment

It is important for users to understand that risk reduction achieved by safety functions is **dependent** on decisions made in design, operation and maintenance



# Questions?

#### **Recommended reading:**

Moubray, J. '*Reliability-centred Maintenance*' Smith, D. J. '*Reliability, Maintainability and Risk*'

